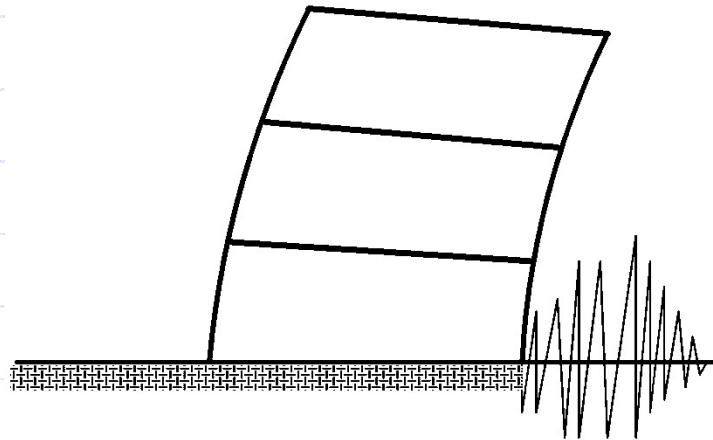


ASCE 7

SEISMIC DESIGN PARAMETERS

WITH 1997 UBC REFERENCE



WIRA TJONG, S.E.

ACKNOWLEDGEMENT

SEVERAL TABLES AND FIGURES ON THIS PRESENTATIONS ARE TAKEN FROM FEMA PUBLICATIONS 274, 412,413,& 414 ,
ICC AND USGS WEB SITES.

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ABBREVIATIONS

➡ **ASCE : AMERICAN SOCIETY OF CIVIL ENGINEERS**

➡ **SEAOC : STRUCTURAL ENGINEER ASSOCIATION OF CALIFORNIA**

➡ **UBC : UNIFORM BUILDING CODES – OLD CODES**

**IBC : INTERNATIONAL BUILDING CODES –
CURRENT CODES WITH REFERENCE TO
ASCE 7 : MINIMUM DESIGN LOADS FOR BUILDING**

**CBC : CALIFORNIA BUILDING CODES – ADOPT IBC
AS BASELINE**



HISTORY OF UBC → IBC

FIRST UBC WAS PUBLISHED IN 1927

SEISMIC PROVISIONS IN APPENDIX & OPTIONAL TO LOCAL JURISDICTION

LONG BEACH EARTHQUAKE IN 1933

CA FIELD ACT : SEISMIC DESIGN MANDATORY FOR SCHOOLS AND, LATER, HOSPITALS

SEISMIC PROVISIONS IN THE MAIN TEXT 1940s

REQUIRED FOR ALL BUILDINGS; PROHIBIT NEW UNREINFORCED MASONRY BUILDINGS; LATE 1940s, MANDATORY BOLTING DOWN OF WOOD FRAME BUILDINGS, INCLUDING HOUSES.

SEISMIC DESIGN REGULATIONS WAS PUBLISHED 1950s

**BY ASCE/SEAOC JOINT COMMITTEE KNOWN AS "SEPARATE 66"
THE FIRST TIME DYNAMIC BEHAVIOR OF STRUCTURE DURING EQ IS CONSIDERED**

HISTORY OF UBC → IBC

SEISMIC DESIGN REGULATIONS WAS FORMED IN 1959
BY SEAOC STATE LEVEL SEISMOLOGY COMMITTEE IN ONGOING
EFFORT FOR BETTER SEISMIC DESIGN CODES

SAN FERNANDO EARTHQUAKE IN 1971
MANY CHANGES IN SEISMIC DESIGN REFLECTED IN 1973 AND 1976
UBC CODES

NEW SEISMIC REQUIREMENTS IN 1973
WALL/ROOF CONNECTIONS FOR TILT UP WALL BUILDING; SOIL
FACTOR; INCREASED FORCE LEVELS (1.5 TO 2.5 TIMES LARGER THAN
PREVIOUS CODES); REQUIRES DUCTILE (SPECIAL) CONCRETE
MOMENT RESISTING FRAMES

MEXICO CITY EARTHQUAKE IN 1985
AMPLIFICATION DUE TO SOFT SOIL

MID 1980s
CA SENATE BILL 547 : UNREINFORCED MASONRY BUILDING RETROFIT
LAW

HISTORY OF UBC → IBC

NEW SEISMIC BASE SHEAR EQUATION IN 1988

CONSIDERATION OF IRREGULAR SHAPES, SIZES AND MASS; GYPSUM BOARD SHEAR CAPACITY WAS REDUCED

LOMA PRIETA EARTHQUAKE IN 1989

AMPLIFICATION IN SOFT SOILS LARGER THAN THE CODE'S EXPECTED

NEW SEISMIC REQUIREMENTS IN 1991

MORE STRINGENT REQUIREMENT FOR BUILDINGS IN SOFT SOILS;
URM RETROFIT STANDARDS IN UCBC APPENDIX CHAPTER 1

NEW SEISMIC REQUIREMENTS IN 1994

USE OF WOOD FRAME CONSTRUCTION WAS DEFINED AND LIMITED;
NEW CONCRETE SHEAR WALL DESIGN REQUIREMENT.

NORTHRIDGE EARTHQUAKE IN 1994

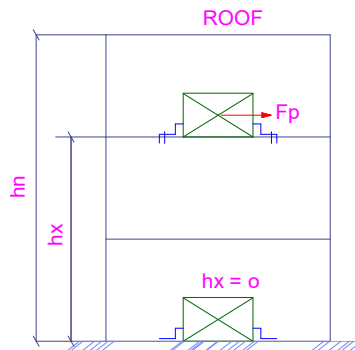
REFLECTED IN 1997 UBC; MORE STRINGENT WALL TO ROOF CONNECTION

MAJOR CHANGES DUE TO RECENT EARTHQUAKE

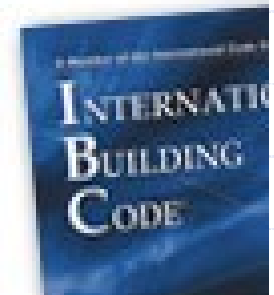
THE LAST UBC - 1997



- ◆ INFLUENCED BY 1994 LOS ANGELES, NORTHRIDGE EQ
- ◆ REDUNDANCY & NEAR FAULT FACTORS
- ◆ R_w WAS REPLACED BY $R = R_w/1.4$ - STRENGTH DESIGN FORMAT
- ◆ VERTICAL SEISMIC FORCE TO BE INCLUDED IN THE DESIGN
- ◆ EQUIPMENT ANCHORAGE BASED ON THE LOCATION ABOVE THE GROUND



ASCE 7



- ◆ EARTHQUAKE FORCES PER ASCE 7 – 2005 OR 2010
- ◆ DESIGN EQ/ BASIS GROUND MOTION
- ◆ SEISMIC ZONES ARE REPLACED BY RESPONSES CONTOUR
- ◆ SEISMIC DESIGN CATEGORY (SDC) & SITE SPECIFIC LONG PERIOD
- ◆ EQUIPMENT ANCHORAGE FORCE REFINEMENT

May 21, 2024

ASCE 7

INTRODUCTION

1A-6

OBJECTIVES & EQ LEVEL DEFINITIONS

1997 UBC

A. TO PROVIDE BUILDING WHICH IS EXPECTED TO MEET **LIFE SAFETY OBJECTIVE AND NOT TO LIMIT DAMAGE OR MAINTAINING FUNCTION**

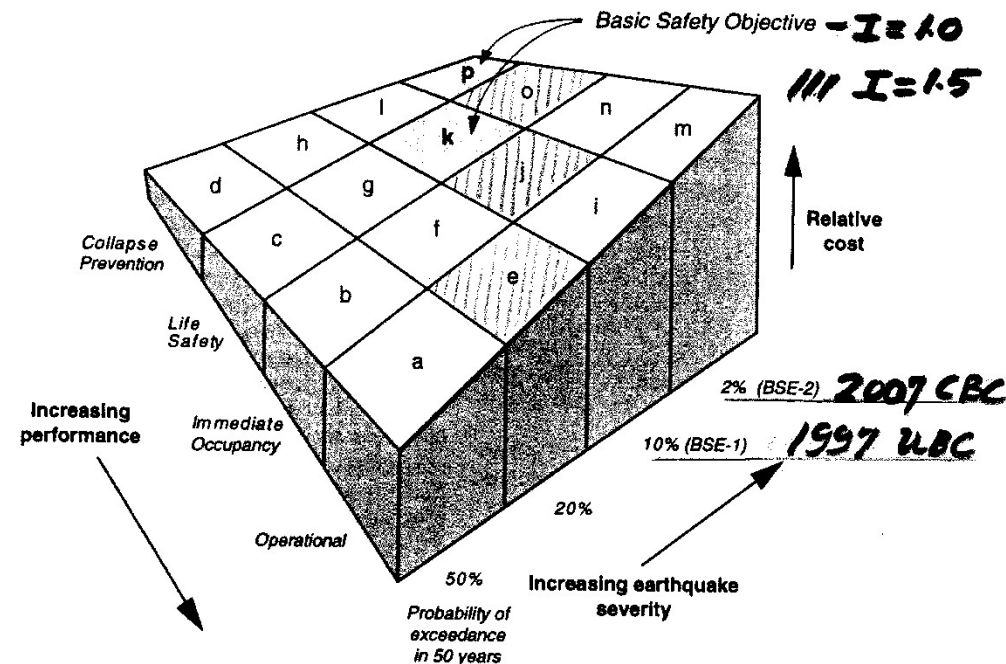
B. STRUCTURES HAVE TO BE ABLE TO RESIST

1. A **MINOR EARTHQUAKE WITHOUT DAMAGE**
2. A **MODERATE EARTHQUAKE WITHOUT STRUCTURAL DAMAGE BUT POSSIBLY EXPERIENCE SOME NON-STRUCTURAL DAMAGE**

ASCE 7

A. **LIFE SAFETY FOR STANDARD BUILDING UNDER DESIGN EARTHQUAKE**

B. **DEFINE EQ LEVEL BASED ON PROBABILITY OF OCCURRENCE**



OBJECTIVES & DESIGN CATEGORY

1997 UBC

3. A **MAJOR EARTHQUAKE** HAVING AN INTENSITY EQUAL TO THE STRONGEST EITHER EXPERIENCED OR FORECAST FOR THE BUILDING **WITHOUT COLLAPSE**, BUT POSSIBLY WITH SOME STRUCTURAL & NON-STRUCTURAL DAMAGE.

IT IS EXPECTED THAT IN MAJOR EARTHQUAKE, DAMAGE WILL BE LIMITED TO **A REPAIRABLE LEVEL**.

ASCE 7

BY CORRELATING THE EXPECTED PERFORMANCE LEVEL UNDER DIFFERENT EQ LEVELS, EACH BUILDING IS ASSIGNED SEISMIC DESIGN CATEGORY (SDC) "A" TO "F" BASED ON

- ◆ **OCCUPANCY CATEGORY OF THE BUILDING**
- ◆ **LOCAL GROUND MOTION INTENSITY AND SITE CLASS/SOIL TYPE**

EACH DESIGN CATEGORY HAS SPECIFIC DETAILING & CONFIGURATION REQUIREMENT WITH CATEGORY "F" AS THE MOST STRINGENT AND DUCTILE.

11.1.2 SCOPE

1997 UBC

- ◆ APPLIES TO BUILDING AND NON- BUILDING STRUCTURES.
- ◆ ONE OR TWO STORY FAMILY DWELLING IN ZONE 1 NEED NOT CONFORM TO THIS PROVISION.



ASCE 7

**EVERY STRUCTURE INCL
NON-STRUCTURAL
COMPONENTS EXCEPT**

- **DETACHED ONE OR TWO
FAMILY DWELLINGS**
 - **UNDER SEISMIC DESIGN
CATEGORY (SDC) A, B, or
C or LOCATED AT THE
AREA WITH $S_s < 0.4 G$**
- OR
 - **ASCE 7: 2 STORIES or
LESS USING WOOD
FRAME SATISFYING IRC**
 - **CBC: SEISMIC RESISTING
SYSTEM OF WOOD FRAME
CONFORMING TO
SECTION 2308**

11.1.2 SCOPE

ASCE 7



- **AGRICULTURAL STORAGE WITH INCIDENTAL HUMAN OCCUPANCY**
- **NOT IN SCOPE SPECIAL STRUCTURES: BRIDGES, ELEC TRANSMISSION TOWERS, BURIED UTILITIES LINES, NUCLEAR REACTORS**



SEISMIC DESIGN REQUIREMENT

- ➔ **SEISMIC DESIGN IS NOT ONLY FOR HIGHRISE BUILDING**
- ➔ **CASUALTY FROM INDUSTRIAL BUILDING FAILURE CAN BE CATASTROPHIC AND ENORMOUS TO THE PUBLIC**
- ➔ **EQUIPMENT ANCHORAGE NEEDS TO BE ENGINEERED AND DESIGNED**
- ➔ **PROPER DETAILING IS MORE IMPORTANT THAN DESIGN FORCES IN SURVIVING SEISMIC EVENT**

OCCUPANCY CATEGORY & IMPORTANCE FACTORS

OCCUPANCY CATEGORY

CBC TABLE 1604.5/ASCE TABLE 1.5 -1

I : OTHER BLDGS/STRUCTURES WITH LOW HAZARD

II : ALL BUILDINGS NOT UNDER I, III, OR IV

III : BUILDINGS WITH SUBSTANTIAL HAZARD AND ECONOMIC IMPACT, MASS DISRUPTION

IV: ESSENTIAL BUILDINGS AND BUILDINGS CONTAINING CERTAIN QUANTITY OF HIGHLY TOXIC SUBSTANCES

BUILDING IMPORTANCE FACTOR

ASCE 7 TABLE 1.5 -2

OC	I	II	III	IV
I	1.0	1.0	1.25	1.50

20.3 SOILS TYPE/SITE CLASS

1997 UBC

SOIL PROFILE TYPE PER TABLE
16-J (6 TYPES)

- USE TYPE **S_d** IF UNKNOWN
- SPECIAL SITE EVALUATION FOR SOIL TYPE **S_f**

ASCE 7

SITE CLASSIFICATION PER
TABLE 20.3-1 (6 CLASSES)


- ◆ USE SITE CLASS **"D"** IF UNKNOWN
- ◆ SPECIAL SITE EVALUATION FOR SITE CLASS **"F"**

Site Class		Shear Wave Velocity
A	Hard rock	> 5000 ft/sec
B	Rock	2,500 to 5,000 ft/sec
C	Very dense soil and soft rock	1,200 to 2,500 ft/sec
D	Stiff soil	600 to 1,200 ft/sec
E	Soft clay soil	< 600 ft/sec
F	Soils vulnerable to failure or collapse under seismic loading, such as liquefiable soils, highly sensitive clays, and weakly cemented soils; require site response analysis in accordance with ASCE 7 Chapter 21.	

SOILS TYPE/SITE CLASS

1997 UBC

SOIL TYPE

Sa Sb Sc Sd Se Sf
 HARD ROCK  SOFT SOIL

TYPE Sf

- ◆ LIQUEFIABLE SOILS, QUICK AND HIGHLY SENSITIVE CLAYS, WEAK CEMENTED SOILS
- ◆ > 10 ft [3 m] THICK PEATS OR HIGHLY ORGANIC CLAY
- ◆ > 25 ft [7.6 m] THICK VERY HIGH PLASTICITY CLAY WITH $PI > 75$
- ◆ > 120 ft [36.5 m] THICK SOFT/MEDIUM STIFF CLAY

ASCE 7

SITE CLASSIFICATION

A B C D E F
 HARD ROCK  SOFT SOIL

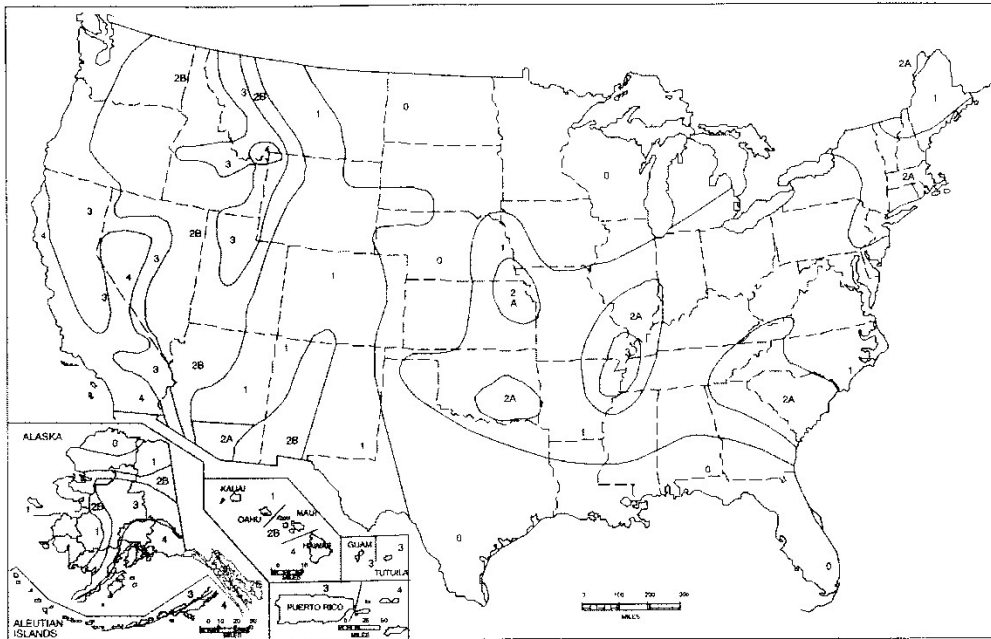
CLASS "F"

- ◆ LIQUEFIABLE SOILS, QUICK AND HIGHLY SENSITIVE CLAYS, WEAK CEMENTED SOILS
- ◆ > 10 ft [3 m] THICK PEATS OR HIGHLY ORGANIC CLAY
- ◆ > 25 ft [7.6 m] THICK VERY HIGH PLASTICITY CLAY WITH $PI > 75$
- ◆ > 120 ft [36.5 m] THICK SOFT/MEDIUM STIFF CLAY

DESIGN EQ GROUND MOTION

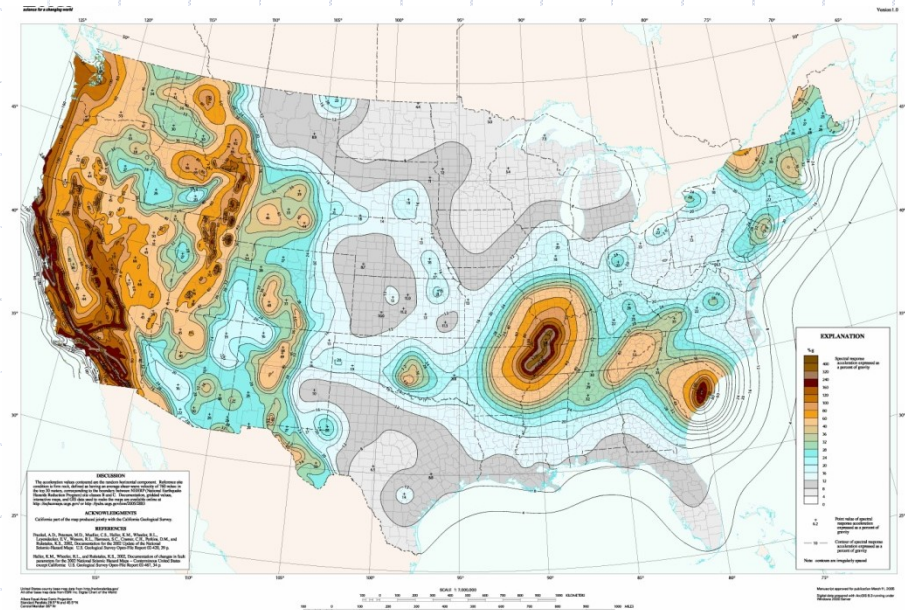
1997 UBC

1. BASIS GROUND MOTION WITH 10% PROBABILITY OF EXCEEDANCE IN 50 YEARS (ONCE IN 475 YEARS)



ASCE 7

1. MAPPED MAX CONSIDERED EQ GEOMETRIC MEAN (MCE_g) PEAK GROUND ACCELERATION WITH 2 % PROBABILITY OF EXCEEDANCE IN 50 YEARS (ONCE IN 2500 +- YEARS)



DESIGN EQ GROUND MOTION

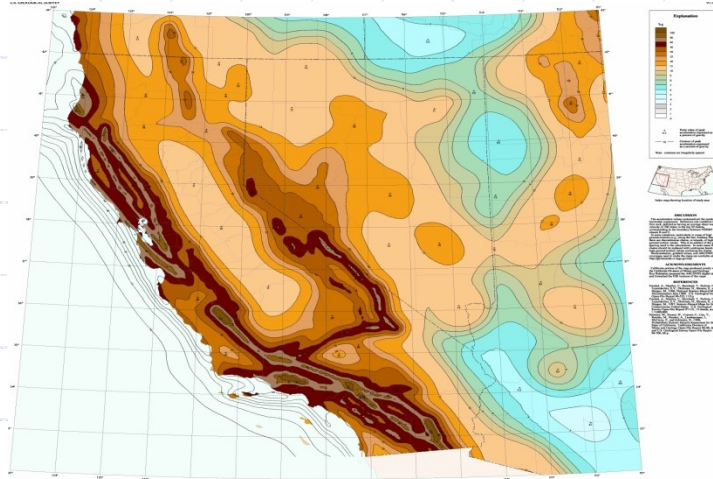
1997 UBC

2. SEISMIC ZONE IN ACCORDANCE WITH FIG. 16-2 WITH A ZONE FACTOR Z PER TABLE 16-I (5 ZONES)

ZONE	1	2A	2B	3	4
Z	0.075	0.15	0.20	0.30	0.40

EFFECTIVE PEAK GROUND ACCELERATION IN g

PGA FOR 475 YEARS EQ



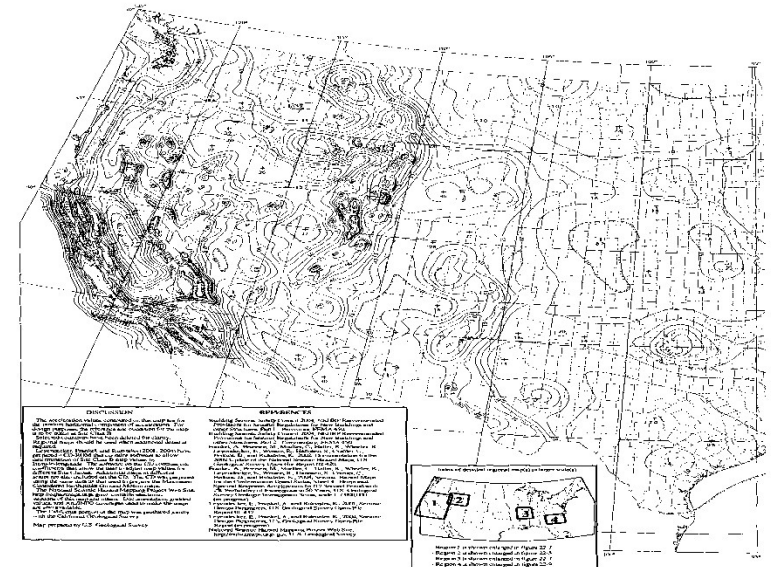
SEISMIC HAZARD MAP FOR CALIFORNIA, NEVADA AND WESTERN ARIZONA/UTAH
MAP A - PEAK HORIZONTAL ACCELERATION

May 21, 2024
ASCE 7

INTRODUCTION

ASCE 7

2. SPECTRAL RESPONSE ACCELERATIONS AT SHORT PERIOD (S_s) AND AT 1 SECOND PERIOD (S_1) BASED ON LOCAL MCE_R WITH 5 % DAMPING



S_s FOR 2500 YEARS EQ

1A-16

SITE COEFFICIENTS

1997 UBC

3. NEAR FAULT FACTORS N_a &
 N_v

ASCE 7

3. DETERMINE SITE
COEFFICIENTS F_a & F_v
PER TABLE 11.4-1 & 2
FUNCTION OF SITE CLASS
& MCE_R SPECTRAL RESP
ACCELERATION S_s AND
 S_1 ON CHAPTER 22

SITE COEFFICIENTS

SITE COEFFICIENT F_a

Linear interpolation for
intermediate
values of S_s and S_1

SITE
C
L
A
S
S

SITE COEFFICIENT F_v

S_s						S_1				
≤ 0.25	0.50	0.75	1.0	≥ 1.25		≤ 0.10	0.2	0.3	0.4	≥ 0.5
0.80	0.80	0.80	0.80	0.80	A	0.80	0.80	0.80	0.80	0.80
1.00	1.00	1.00	1.00	1.00	B	1.00	1.00	1.00	1.00	1.00
1.20	1.20	1.10	1.00	1.00	C	1.70	1.60	1.50	1.40	1.30
1.60	1.40	1.20	1.10	1.00	D	2.40	2.00	1.80	1.60	1.50
2.50	1.70	1.20	0.90	0.90	E	3.50	3.20	2.80	2.40	2.40

DESIGN SPECTRAL RESPONSES

1997 UBC

4. BASED ON ZONE AND SOIL PROFILE, DETERMINE SEISMIC RESPONSE COEFFICIENTS C_a PER TABLE 16 - Q AND C_v PER TABLE 16 - R
5. FOR ZONE 4, DETERMINE THE NEAR FAULT FACTORS N_a AND N_v BASED ON DISTANCE FROM AND THE TYPE OF THE NEARBY FAULT.

ASCE 7

4. DETERMINE RISK TARGETED MAX CONSIDERED EQ (MCE_R) SPECTRAL RESPONSE ACCELERATION PARAMETERS

$$S_{ms} = F_a S_s$$

$$S_{m1} = F_v S_1$$

5. DETERMINE DESIGN SPECTRAL RESPONSE ACCELERATION PARAMETERS

$$SD_s = 2/3 S_{ms}$$

$$SD_1 = 2/3 S_{m1}$$

$$SD_s = 2.5 C_a \text{ \& } SD_1 = C_v$$

11.6 SEISMIC DESIGN CATEGORY(SDC)

SDC IS USED TO DETERMINE THE REQUIRED LEVEL OF DUCTILE DETAILING & PERMITTED STRUCTURE CONFIGURATION

TABLES 1613.5.6(1) / ASCE 7 – 11.6.1

- 1. DETERMINE SEISMIC DESIGN CATEGORY (SDC "A" TO "F") PER CBC SECTION 1613.5.6 OR ASCE 7 11.6. USE THE MOST SEVERE SDC FROM THE TABLES REGARDLESS OF T**

OCCUPANCY CATEGORY

VALUE OF SDs	I or II	III	IV
SDs < 0.167 g	A	A	A
0.167 g ≤ SDs < 0.33 g	B	B	C
0.33 g ≤ SDs < 0.50 g	C	C	D
SDs ≥ 0.50 g	D	D	D

TABLES 1613.5.6(2) / ASCE 7 - 11.6-2

- 2. SDC E FOR OC I TO III AT S1 ≥ 0.75 g**
- 3. SDC F FOR OC IV AT S1 ≥ 0.75 g**

VALUE OF SD1	I or II	III	IV
SD1 < 0.067 g	A	A	A
0.067 g ≤ SD1 < 0.133 g	B	B	C
0.133 g ≤ SD1 < 0.20 g	C	C	D
SD1 ≥ 0.20 g	D	D	D
S1 ≥ 0.75 g	E	E	F



SDC EXAMPLE

SEVEN STORY CONCRETE FRAME FOR OFFICE BUILDING IN KATHMANDU

Acceleration Responses :

$S_s = 1.15 \text{ g}$ & $S_1 = 0.45 \text{ g}$ - US STATE DEPT.

OFFICE BUILDING

Occupancy Category II - $I = 1.0$

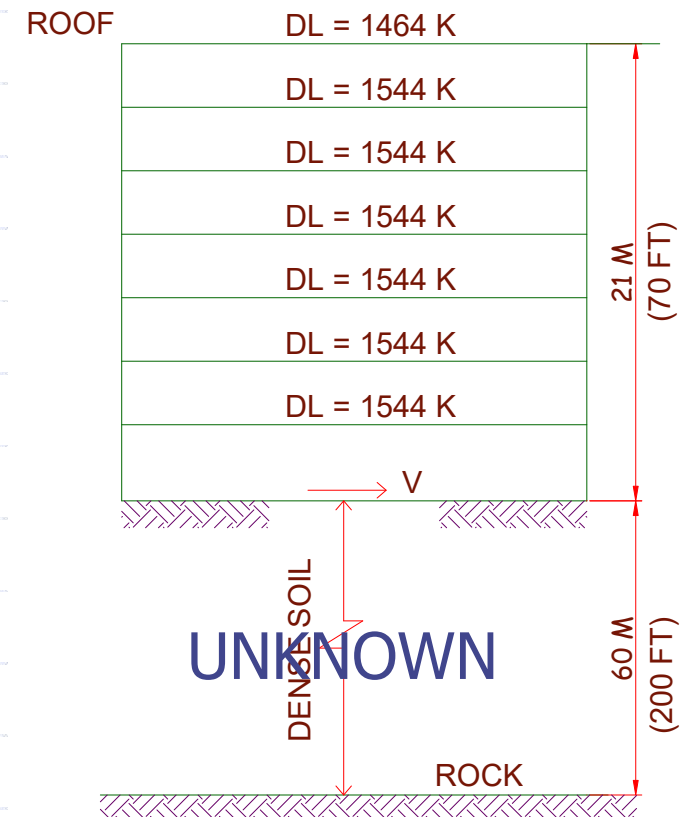
PER TABLE 20.3-1 , UNKNOWN SOILS
CONDITION

SITE CLASS "D"

SITE COEFFICIENTS:

$F_a = 1.01$ FROM TABLE 11.4-1

$F_v = 1.55$ FROM TABLE 11.4-2



SDC EXAMPLE

SPECTRAL ACCELERATION RESPONSE:

$$S_{ms} = F_a S_s = 1.10 \quad ; \quad S_{m1} = F_v S_1 = 0.70$$

DESIGN ACCELERATION RESPONSE:

$$SD_s = 2/3 S_{ms} = 0.80 \quad ; \quad SD_1 = 2/3 S_{m1} = 0.47 \text{ in } g$$

SEISMIC DESIGN CATEGORY:

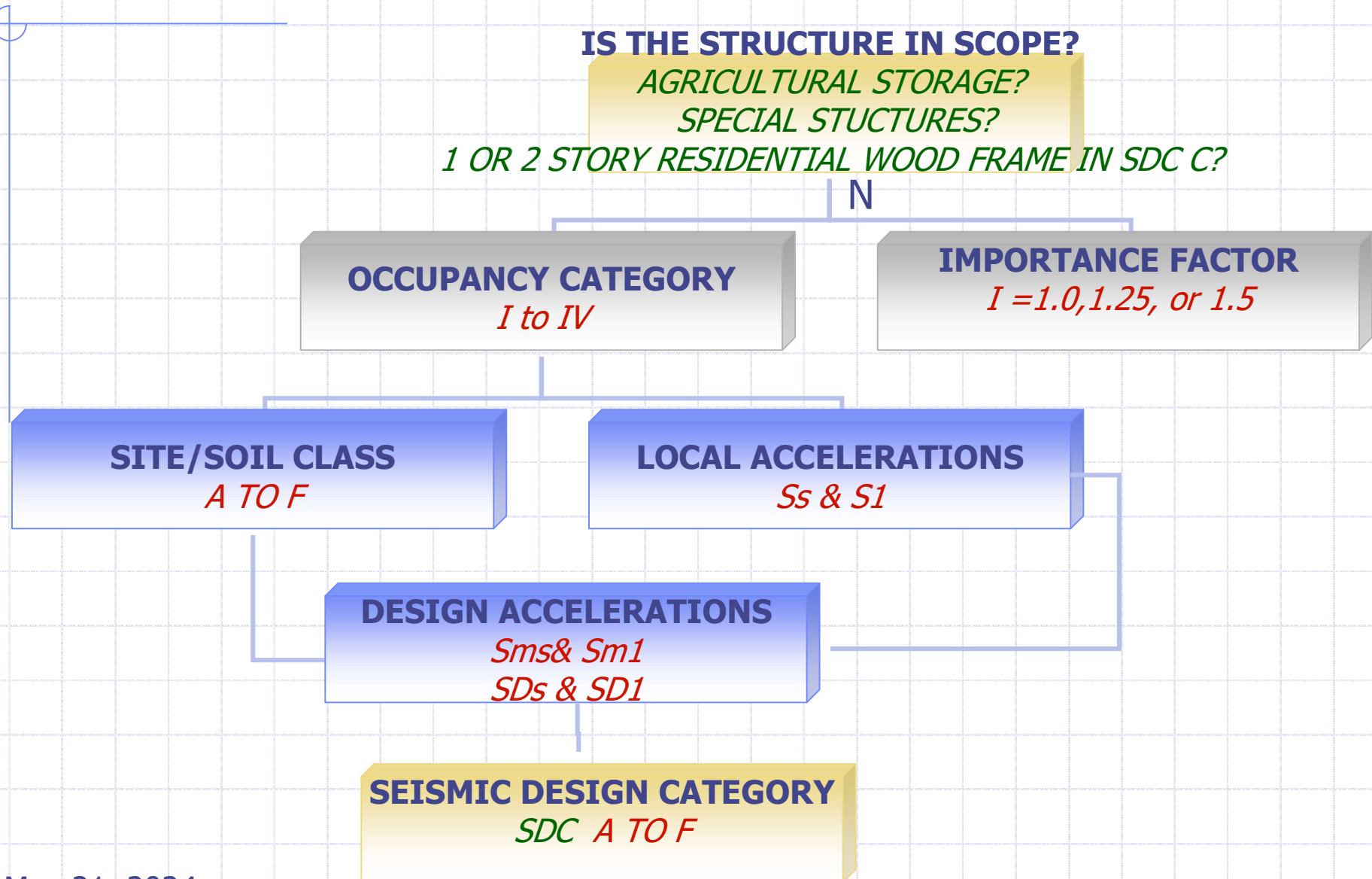
BASED ON THE DESIGN ACCELERATION RESPONSE, TAKE THE WORST WORST CASE FROM TABLES 11.6-1 & 11.6-2 TO GET THE SEISMIC DESIGN CATEGORY:

SDC "D"

CHECK PROVISION FOR $S_1 > 0.75 g$... NOT APPLICABLE

IBCPRO SOFTWARE

SEISMIC DESIGN CATEGORY STEPS SUMMARY



END OF SEMINAR



THANKS ...
QUESTIONS AND
ANSWERS